

Second-order Extension of Hooke's Law in Elasticity Based on a New Boltzmann-type Collision Model

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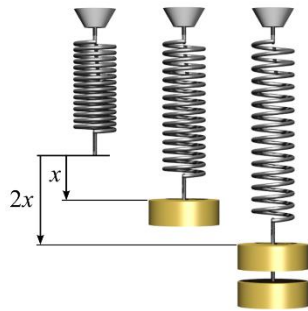
Dr. Satyvir Singh (Graduate Student; now Postdoctoral Researcher in RWTH Aachen Univ.)

Development of hybrid DG code and computational simulation of rarefied & microscale gas flows

Dr. Tushar Chourushi (Graduate Student; now Assistant Professor in Amity University Mumbai)

Development of viscoelastic code and computational simulation of viscoelastic flows

Hooke's law in elasticity (1676)

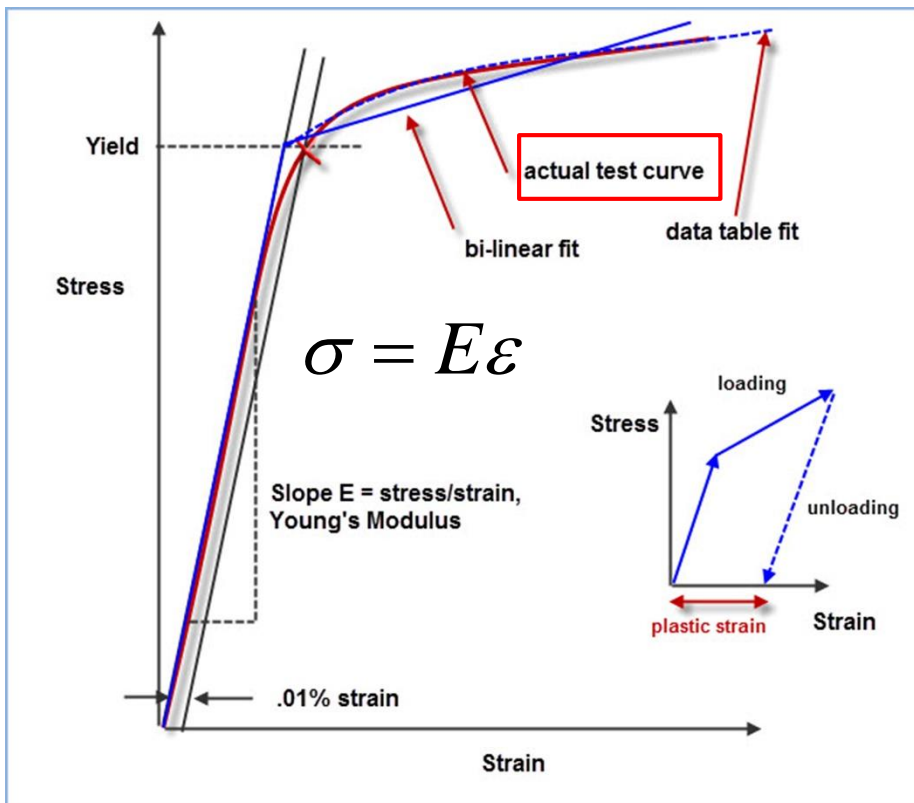


$$F = -kx$$

In the physics and mechanics of elastic solids, **Hooke's law** is an empirical law that states that the force needed to extend or compress a spring is proportional linearly to the distance.

The law is named after 17th-century British physicist **Robert Hooke** who first stated the law in 1676.

Hooke's law is only a **first-order approximation** to the real response of springs and other elastic bodies to applied forces.

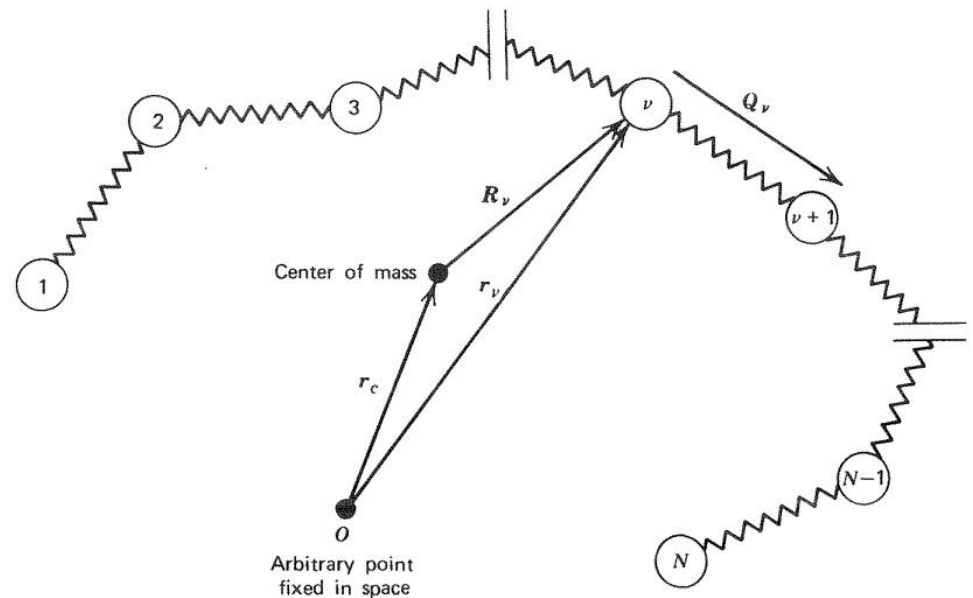
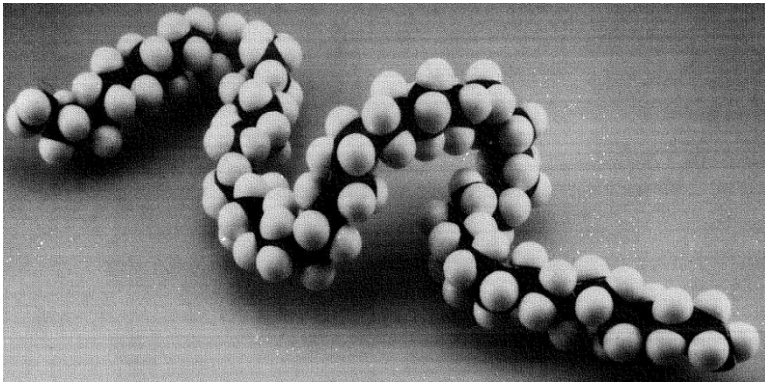


Elastic dumbbell models: kinetic theory of polymers

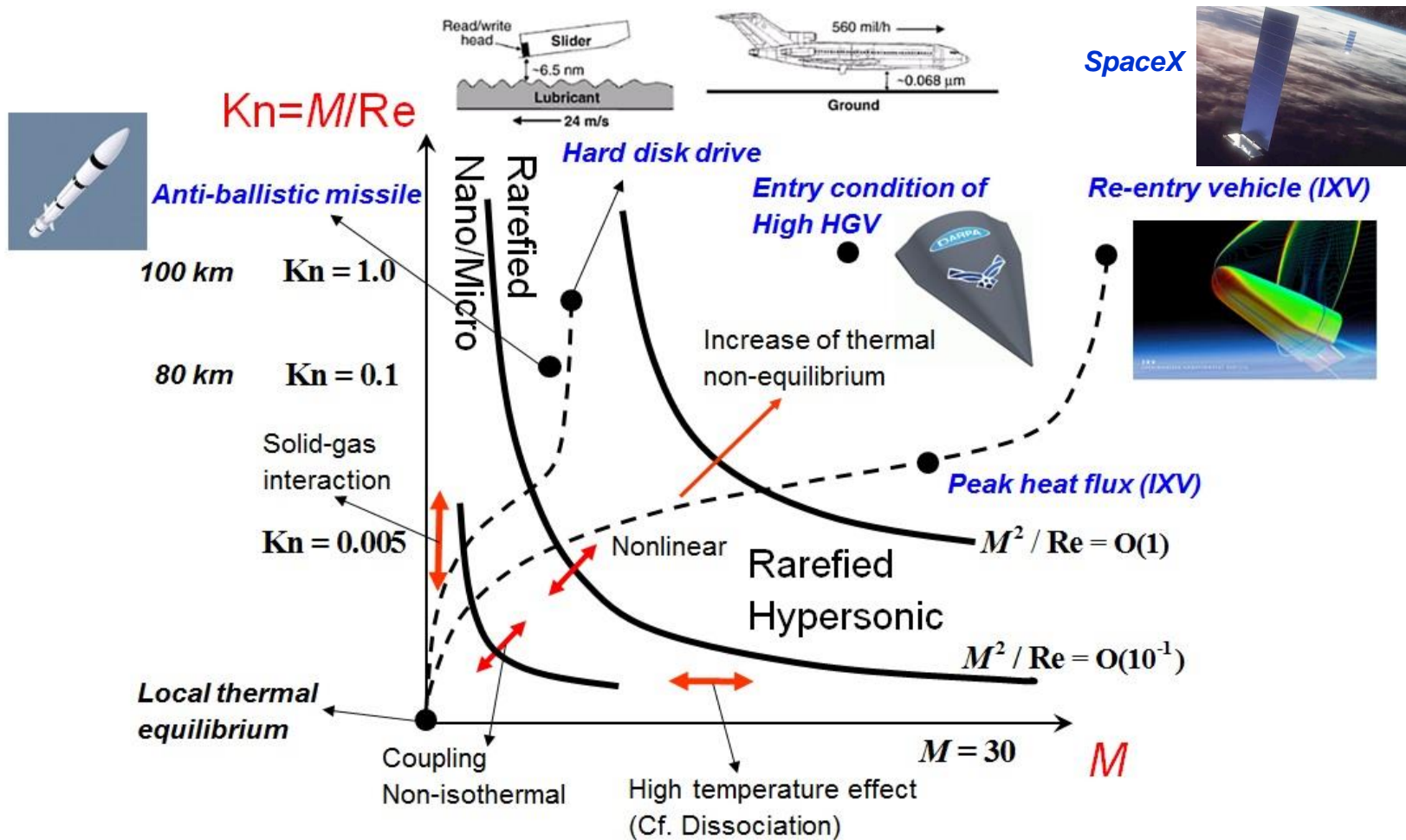
Hyper-elastic materials such as rubber (amorphous solid)



Mostly phenomenological models such as Mooney (1940)–Rivlin (1948) solid model



Classification of gas flows in non-equilibrium



$\mathbf{v} \cdot \nabla f(\mathbf{r}, \mathbf{v}) = C[f, f_2]$ $\xrightarrow[\text{via statistical average}]{M \text{ appearing}}$ $\rho \mathbf{u} \cdot \nabla \mathbf{u} + \nabla \cdot p \mathbf{I} + \nabla \cdot \Pi = 0 \implies$ **Main parameter** $\Pi / p \sim \frac{Kn \cdot M}{Re} \text{ or } \frac{M}{\sqrt{Re}}$

Two terms: Kn Three terms: M, Kn (not Kn alone)

Boltzmann kinetic equations

- A first-order partial differential equation of **the probability density of finding a particle in phase space** with an integral collision term

$$\left(\frac{\partial}{\partial t} + \mathbf{v} \cdot \nabla \right) f(t, \mathbf{r}, \mathbf{v}) = \frac{1}{Kn} C[f, f_2]$$

Movement

Collision (or Interaction)

Kinematic

Dissipation

$$C[f, f_2] \sim \int |\mathbf{v} - \mathbf{v}_2| (f^* f_2^* - ff_2) d\mathbf{v}_2$$

$$= \text{Gain (scattered into)} - \text{Loss (scattered out)} = \left(\frac{\delta f}{\delta t} \right)^+ - \left(\frac{\delta f}{\delta t} \right)^-$$



- Maxwell's equation of transfer** for molecular expression $h^{(n)}$

$$\frac{\partial}{\partial t} \langle h^{(n)} f \rangle + \nabla \cdot \left(\mathbf{u} \langle h^{(n)} f \rangle + \langle \mathbf{c} h^{(n)} f \rangle \right) - \left\langle f \frac{d}{dt} h^{(n)} \right\rangle - \langle f \mathbf{c} \cdot \nabla h^{(n)} \rangle = \langle h^{(n)} C[f, f_2] \rangle$$

Relationship with conservation laws (moments)

Boltzmann transport equation (BTE): 10²³

$$\left(\frac{\partial}{\partial t} + \mathbf{v} \cdot \nabla \right) f(t, \mathbf{r}, \mathbf{v}) = \mathbf{C}[f, f_2]$$

$$\rho \mathbf{u} = \langle m \mathbf{v} f(t, \mathbf{r}, \mathbf{v}) \rangle$$

$$\text{where } \langle \dots \rangle = \iiint \dots dv_x dv_y dv_z$$

Differentiating the statistical definition $\rho \mathbf{u} \equiv \langle m \mathbf{v} f(t, \mathbf{r}, \mathbf{v}) \rangle$ *with time* and *then combining* with BKE ($t, \mathbf{r}, \mathbf{v}$ are independent and $\mathbf{v} = \mathbf{u} + \mathbf{c}$)

$$\frac{\partial}{\partial t} \langle m \mathbf{v} f \rangle = \left\langle m \mathbf{v} \frac{\partial f}{\partial t} \right\rangle = - \langle m (\mathbf{v} \cdot \nabla f) \mathbf{v} \rangle + \langle m \mathbf{v} \mathbf{C}[f, f_2] \rangle$$

$[\mathbf{A}]^{(2)}$: Traceless symmetric part of tensor \mathbf{A}

$$\text{Here } - \langle m (\mathbf{v} \cdot \nabla f) \mathbf{v} \rangle = - \nabla \cdot \langle m \mathbf{v} \mathbf{v} f \rangle = - \nabla \cdot \{ \rho \mathbf{u} \mathbf{u} + \langle m \mathbf{c} \mathbf{c} f \rangle \}$$

After the decomposition of the stress into **pressure** and **viscous shear stress**

$$\mathbf{P} \equiv \langle m \mathbf{c} \mathbf{c} f \rangle = p \mathbf{I} + \mathbf{\Pi} \text{ where } p \equiv \langle m \text{Tr}(\mathbf{c} \mathbf{c}) f / 3 \rangle, \mathbf{\Pi} \equiv \langle m [\mathbf{c} \mathbf{c}]^{(2)} f \rangle,$$

and using the collisional invariance of the momentum, $\langle m \mathbf{v} \mathbf{C}[f, f_2] \rangle = 0$, we have

$$\frac{\partial(\rho \mathbf{u})}{\partial t} + \nabla \cdot (\rho \mathbf{u} \mathbf{u} + p \mathbf{I} + \mathbf{\Pi}) = \mathbf{0}$$

Conservation laws: 13

Closing-last balanced closure on open terms

$$\mathbf{\Pi} \equiv \left\langle m[\mathbf{cc}]^{(2)} f \right\rangle, \mathbf{Q} \equiv \left\langle mc^2 \mathbf{c} / 2f \right\rangle$$

Closure theory: **how, where (open terms), when (last)**

New balanced closure with closure-last approach (PoF 2014)

2nd-order for kinematic LH = 2nd-order for collision RH

$$\begin{aligned} \frac{D}{Dt}(\mathbf{\Pi} / \rho) + \boxed{\nabla \cdot \Psi^{(\Pi)}} + 2[\mathbf{\Pi} \cdot \nabla \mathbf{u}]^{(2)} + 2p[\nabla \mathbf{u}]^{(2)} &= \boxed{\left\langle m[\mathbf{cc}]^{(2)} C[f, f_2] \right\rangle} \\ &\text{2nd-order closure} \qquad \qquad \qquad \text{2nd-order closure} \\ &= -\frac{p}{\mu_{NS}} \mathbf{\Pi} q_{2nd}(\kappa_1) \text{ where } \Psi^{(\Pi)} = \left\langle m\mathbf{cccc}f \right\rangle - \left\langle m\text{Tr}(\mathbf{ccc})f \right\rangle \mathbf{I} / 3 \end{aligned}$$

$$\frac{D}{Dt}(\Psi^{(\Pi)} / \rho) + \nabla \cdot \Xi + \dots = \left\langle h^{(\Psi^{(\Pi)})} C[f, f_2] \right\rangle$$

Other collision operator

Collision operator	$C(f_i, f_j)$
Boltzmann	$\int d\mathbf{u}_j \int_0^\pi d\phi \int_0^\infty db b g_{ij} (f_i^* f_j^* - f_i f_j)$
Vlasov-Landau	$2\pi e_i^2 e_j^2 \ln \Lambda \int d\mathbf{u}' \partial_{ij} \cdot \mathbf{U}'(\mathbf{g}) \cdot \partial_{ij} f_i(\mathbf{u}') f_j(\mathbf{u}')$
Balescu-Lenard	$\sum_{\mathbf{k}} \frac{\pi \omega_i^2 \omega_j^2}{n_i^2 m_i} (\mathbf{k}/k^2) \cdot \partial_{\mathbf{u}} \int d\mathbf{u}' (\mathbf{k}/k^2) \cdot (m_j \partial_{\mathbf{u}} - m_i \partial_{\mathbf{u}'}) f_i(\mathbf{u}) f_j(\mathbf{u}') \frac{\delta(\mathbf{k} \cdot \mathbf{u} - \mathbf{k} \cdot \mathbf{u}')}{ \epsilon(\mathbf{k}, \mathbf{k} \cdot \mathbf{u}) ^2}$
Fokker-Planck	$-2\pi e_i^2 e_j^2 m_i^{-1} \ln \Lambda \partial_{u\alpha} \int d\mathbf{u}' [f_i(\mathbf{u}) \partial_{u'\beta} f_j(\mathbf{u}')/m_j - f_j(\mathbf{u}') \partial_{u'\beta} f_i(\mathbf{u})] U_{\alpha\beta}(\mathbf{u} - \mathbf{u}')$
$U'_{\alpha\beta}(\mathbf{x}) = x^{-3}(x^2 \delta_{\alpha\beta} - x_\alpha x_\beta); \quad \partial_{ij} = m_i^{-1} \partial_{\mathbf{u}} - m_j^{-1} \partial_{\mathbf{u}'}; \quad \mathbf{g} = \mathbf{u} - \mathbf{u}';$	
$\omega_i^2 = 4\pi n_i e_i^2 / m_i; \quad \ln \Lambda = \text{Coulomb logarithm};$	
$\epsilon(\mathbf{k}, \omega) = 1 + \sum_I (\omega_i^2 / k^2) \int d\mathbf{u} (\omega - \mathbf{k} \cdot \mathbf{u}) \mathbf{k} \cdot \partial_{\mathbf{u}} f_i(\mathbf{u}).$	

If there are no external forces, and conditions are uniform throughout the gas, this equation takes the form (equation (16)):

Boltzmann

$$\frac{\partial f(x, t)}{\partial t} = \int_0^\infty \int_0^{x+x'} \left[\frac{f(\xi, t) f(x+x'-\xi, t)}{\sqrt{\xi} \sqrt{(x+x'-\xi)}} - \frac{f(x, t) f(x', t)}{\sqrt{x} \sqrt{x'}} \right] \sqrt{(xx')} \psi(x, x', \xi) dx' d\xi$$

(1872)

where the variables x and x' denote the energies of two molecules before a collision, and ξ and $(x+x'-\xi)$ denote their energies after the collision; $\psi(x, x', \xi)$ is a function which depends on the nature of the forces between the molecules.

Closure of dissipation terms via 2nd-law

Key ideas; exponential canonical form, consideration of entropy production σ , and non-polynomial expansion called as cumulant expansion (B. C. Eu in 80-90s)

By writing the distribution function f in the exponential form

$$f = \exp \left[-\beta \left(\frac{1}{2} mc^2 + \sum_{n=1}^{\infty} X^{(n)} h^{(n)} - N \right) \right], \quad \beta \equiv \frac{1}{k_B T},$$

Nonequilibrium entropy Ψ : $\Psi(\mathbf{r}, t) = -k_B \langle [\ln f(\mathbf{v}, \mathbf{r}, t) - 1] f(\mathbf{v}, \mathbf{r}, t) \rangle$,

Nonequilibrium entropy production: $\sigma_c \equiv -k_B \langle \ln f \mathcal{C}[f, f_2] \rangle \geq 0$ (satisfying 2nd-law)

$\sigma_c = \kappa_1 q(\kappa_1^{(\pm)}, \kappa_2^{(\pm)}, \dots)$ via cumulant expansion

$$\sigma_c \equiv -k_B \langle \ln f \mathcal{C}[f, f_2] \rangle = \frac{1}{T} \sum_{n=1}^{\infty} X^{(n)} \langle h^{(n)} \mathcal{C}[f, f_2] \rangle = \frac{1}{T} \sum_{l=1}^{\infty} X^{(n)} \Lambda^{(n)},$$

a thermodynamically-consistent constitutive equation, still exact to BKE, can be derived;

$$\rho \frac{D(\Pi / \rho)}{Dt} + \nabla \cdot \Psi^{(\Pi)} + 2[\Pi \cdot \nabla \mathbf{u}]^{(2)} + 2p[\nabla \mathbf{u}]^{(2)} = \frac{1}{\beta g} \sum_{l=1}^{\infty} R_{12}^{(2l)} X_2^{(l)} q(\kappa_1^{(\pm)}, \kappa_2^{(\pm)}, \dots)$$

Note: When f is truncated to a finite number of terms, the set is truncated in such a way that the divergence problem would not arise.

Cumulant expansion method

$$\langle x^l \rangle = \int x^l f(x) dx, \quad \langle e^{\lambda x} \rangle = \int e^{\lambda x} f(x) dx$$

Then we have

$$\langle e^{\lambda x} \rangle = \sum_{l=0}^{\infty} \frac{\lambda^l}{l!} \langle x^l \rangle = \exp \left[\sum_{l=1}^{\infty} \frac{\lambda^l}{l!} \kappa_l \right] \text{ where}$$

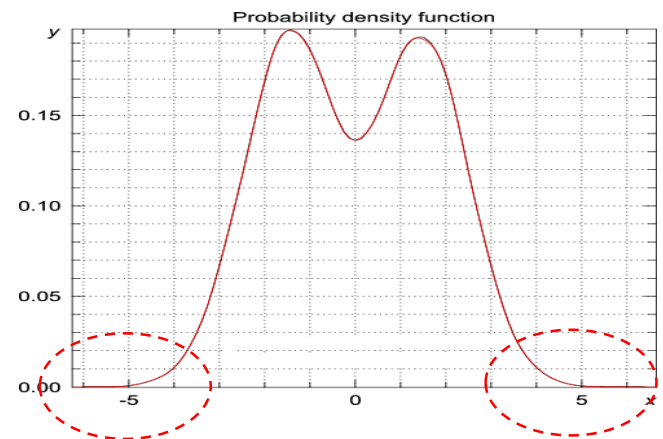
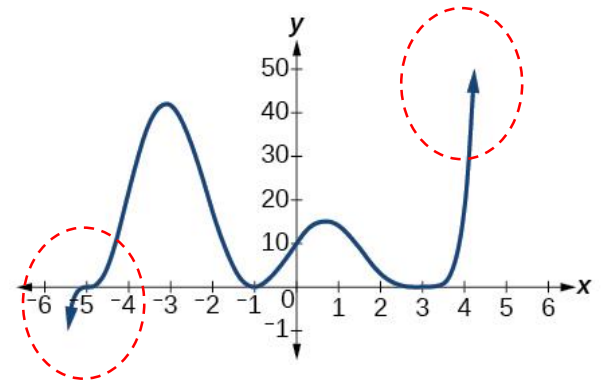
$$\kappa_l = \left[\frac{d^l}{d\lambda^l} \ln \langle e^{\lambda x} \rangle \right]_{\lambda=0} ; \quad \kappa_1 = \langle x \rangle, \quad \kappa_2 = \langle x^2 \rangle - \langle x \rangle^2, \dots \text{ (mean, variance)}$$

$$\langle e^x \rangle_{\text{polynomial}} = 1 + \langle x \rangle + \frac{1}{2!} \langle x^2 \rangle + \frac{1}{3!} \langle x^3 \rangle + \dots,$$

$$\langle e^x \rangle_{\text{cumulant}} = \exp \left[\langle x \rangle + \frac{1}{2!} (\langle x^2 \rangle - \langle x \rangle^2) + \dots \right]$$

$$\left[\frac{\langle e^x \rangle - \langle e^{-x} \rangle}{2} \right]_{\text{polynomial}} = \langle x \rangle + \frac{1}{3} \langle x^3 \rangle + \dots \approx \langle x \rangle$$

$$\left[\frac{\langle e^x \rangle - \langle e^{-x} \rangle}{2} \right]_{\text{cumulant}} = \exp \left(\frac{1}{2!} (\langle x^2 \rangle - \langle x \rangle^2) + \dots \right) \left[\exp(\langle x \rangle + \dots) - \exp(-\langle x \rangle + \dots) \right] / 2 \approx \sinh \langle x \rangle$$



Conservation laws (exact consequence of BKE)

$$\frac{\partial(\rho\mathbf{u})}{\partial t} + \nabla \cdot (\rho\mathbf{u}\mathbf{u} + p\mathbf{I} + \mathbf{\Pi}) = \mathbf{0}$$

in conjunction with the **2nd-order constitutive relations (CR)**

$$\frac{\partial \mathbf{\Pi}}{\partial t} + \mathbf{u} \cdot \nabla \mathbf{\Pi} + \nabla \cdot \Psi^{(\mathbf{\Pi})} + 2[\mathbf{\Pi} \cdot \nabla \mathbf{u}]^{(2)} + 2p[\nabla \mathbf{u}]^{(2)} = -\frac{p}{\mu_{NS}} \mathbf{\Pi} q_{2nd}(\kappa_1),$$

Zero in 2nd-order approximation
Non-local term 2nd-order coupling Navier 1st law

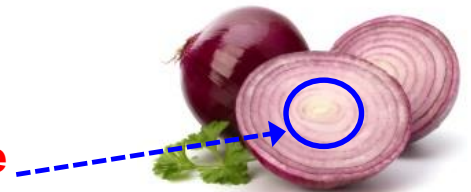
$$\Psi^{(\mathbf{\Pi})} \equiv \langle m\mathbf{c}\mathbf{c}\mathbf{c}f \rangle - \langle m\text{Tr}(\mathbf{c}\mathbf{c}\mathbf{c})f \rangle \mathbf{I} / 3$$

$$q_{2nd}(\kappa_1) \equiv \frac{\sinh \kappa_1}{\kappa_1}, \quad \kappa_1 \equiv \frac{T^{1/4}}{p} \left(\frac{\mathbf{\Pi} : \mathbf{\Pi}}{\mu_{NS}} + \frac{\mathbf{Q} \cdot \mathbf{Q} / T}{k_{NS}} \right)^{1/2}$$

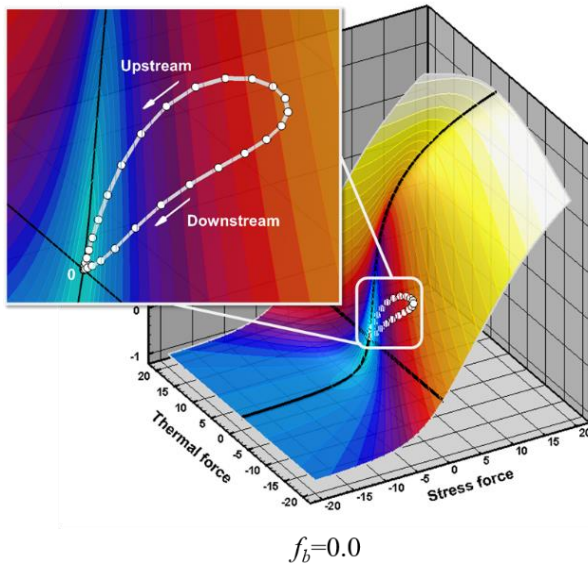
Onsager-Rayleigh
dissipation function

Sinh{1st-order theory}

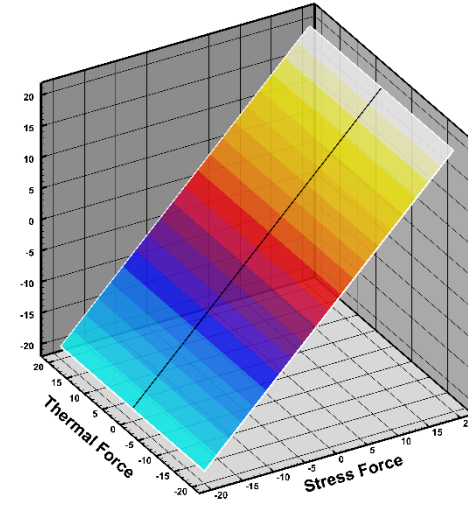
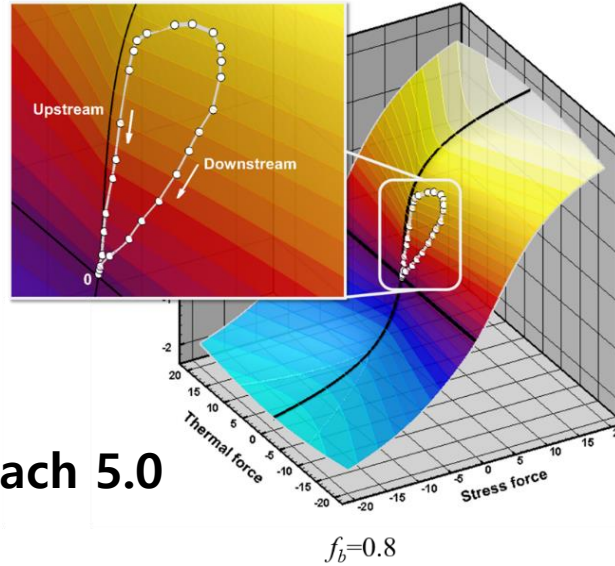
**Navier-Fourier laws inclusive
like onion!**



Topology of 2nd-order NCCR (shock structure) (PoF 2020)



Mach 5.0



$$\left[\hat{\Pi} \cdot \nabla \hat{\mathbf{u}} \right]^{(2)} + (1 + f_b \hat{\Delta}) \hat{\Pi}_0 = \hat{\Pi} q_{2nd}(c\hat{R}), \quad (\text{shear stress})$$

$$\frac{3}{2} (\hat{\Pi} + f_b \hat{\Delta} \mathbf{I}) : \nabla \hat{\mathbf{u}} + \hat{\Delta}_0 = \hat{\Delta} q_{2nd}(c\hat{R}), \quad (\text{excess normal stress})$$

$$\hat{\Pi} \cdot \hat{\mathbf{Q}}_0 + (1 + f_b \hat{\Delta}) \hat{\mathbf{Q}}_0 = \hat{\mathbf{Q}} q_{2nd}(c\hat{R}), \quad (\text{heat flux})$$

where $\hat{R}^2 \equiv \hat{\Pi} : \hat{\Pi} + (5 - 3\gamma) f_b \hat{\Delta}^2 + \hat{\mathbf{Q}} \cdot \hat{\mathbf{Q}}$ (Onsager-Rayleigh dissipation function)

$$\Delta = \left\langle m \text{Tr}(\mathbf{cc}) f / 3 - m \text{Tr}(\mathbf{cc}) f^{(0)} / 3 \right\rangle, \quad p = \left\langle m \text{Tr}(\mathbf{cc}) f^{(0)} / 3 \right\rangle$$

$$\hat{\Pi}_0 = -2\mu [\nabla \mathbf{u}]^{(2)}$$

$$\hat{\Delta}_0 = -\mu_b \nabla \cdot \mathbf{u}$$

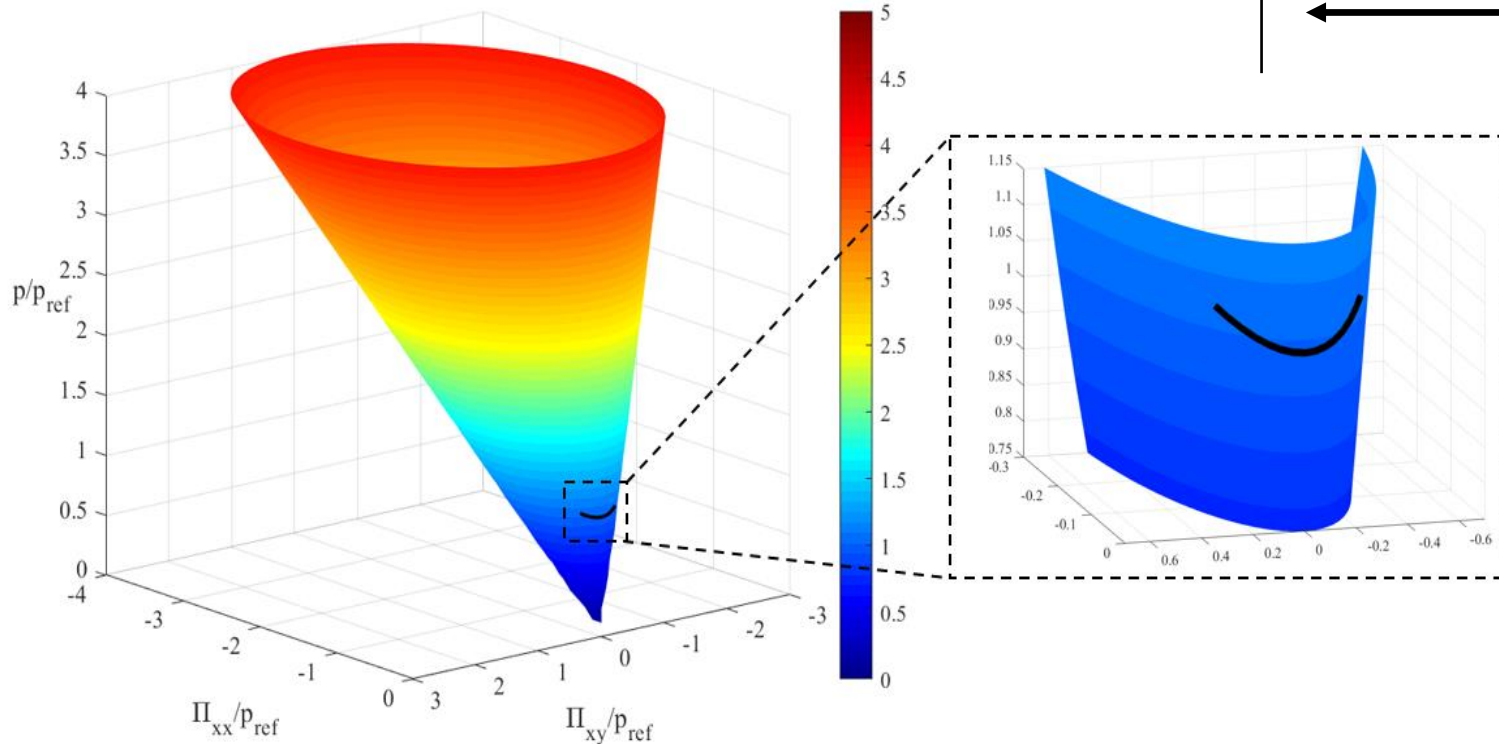
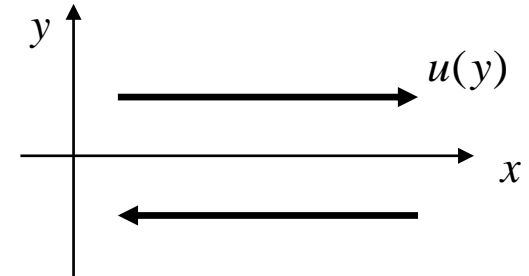
$$\hat{\mathbf{Q}}_0 = -k \nabla T$$

Topology of 2nd-order NCCR (velocity shear) (PoF 2016)

$$\mathbf{u} \cdot \nabla \Pi + 2[\Pi \cdot \nabla \mathbf{u}]^{(2)} + 2p[\nabla \mathbf{u}]^{(2)} = -\frac{p}{\mu_{NS}} \Pi q_{2nd}(\kappa_1)$$

Zero in velocity shear

$$\left(\frac{\Pi_{xy}}{p}\right)^2 = -\frac{3}{2} \left(1 + \frac{\Pi_{yy}}{p}\right) \frac{\Pi_{yy}}{p}$$



3D mixed modal DG method for the 2nd-order model

$$\partial_t \mathbf{U} + \nabla \mathbf{F}_{\text{inv}}(\mathbf{U}) + \nabla \mathbf{F}_{\text{vis}}(\mathbf{U}, \nabla \mathbf{U}) = 0$$

Discretization in **mixed form**

$$\begin{cases} \mathbf{S} - \nabla \mathbf{U} = 0 \\ \partial_t \mathbf{U} + \nabla \mathbf{F}_{\text{inv}}(\mathbf{U}) + \nabla \mathbf{F}_{\text{vis}}(\mathbf{U}, \mathbf{S}) = 0 \end{cases}$$

JCP 2022

NSF model $(\mathbf{\Pi}, \mathbf{Q}) = \mathbf{f}_{\text{linear}}(\mathbf{S}(\mathbf{U}))$

NCCR model $(\mathbf{\Pi}, \mathbf{Q})_{\text{NCCR}} = \mathbf{f}_{\text{non-linear}}(\mathbf{S}(\mathbf{U}), p, T)$

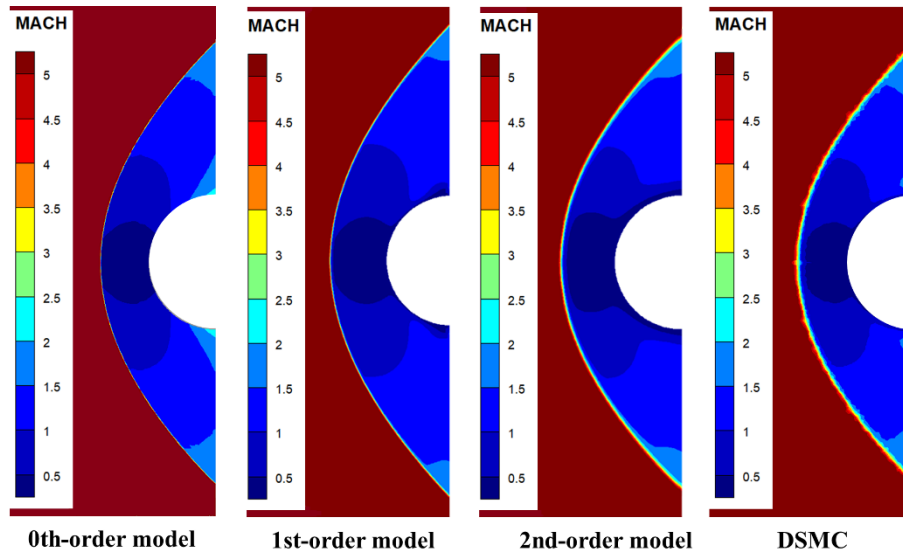
NCCR: Nonlinear Coupled
Constitutive Relation

$$\mathbf{U}_h(\mathbf{x}, t) = \sum_{i=0}^k U_j^i(t) \varphi^i(\mathbf{x}), \quad \mathbf{S}_h(\mathbf{x}, t) = \sum_{i=0}^k S_j^i(t) \varphi^i(\mathbf{x})$$

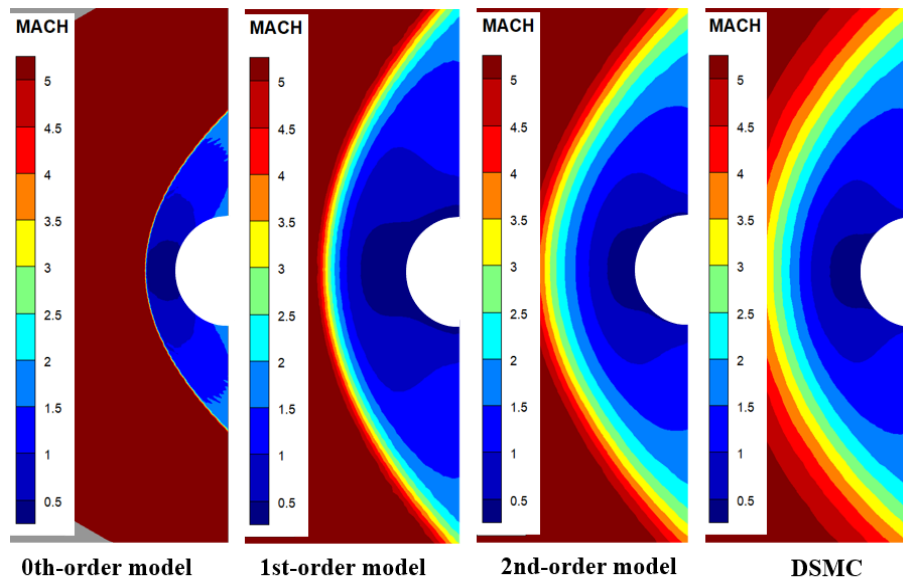
$$\begin{cases} \frac{\partial}{\partial t} \int_I \mathbf{U} \varphi dV - \int_I \nabla \varphi \mathbf{F}_{\text{inv}} dV + \int_{\partial I} \varphi \mathbf{F}_{\text{inv}} \cdot \mathbf{n} d\Gamma - \int_I \nabla \varphi \mathbf{F}_{\text{vis}} dV + \int_{\partial I} \varphi \mathbf{F}_{\text{vis}} \cdot \mathbf{n} d\Gamma = 0, \\ \int_I \mathbf{S} \varphi dV + \int_I T^s \nabla \varphi \mathbf{U} dV - \int_{\partial I} T^s \varphi \mathbf{U} \cdot \mathbf{n} d\Gamma = 0, \end{cases}$$

Dubiner basis function, Lax-Friedrichs inviscid flux, central flux for viscous terms

2-D hypersonic rarefied flow past a cylinder



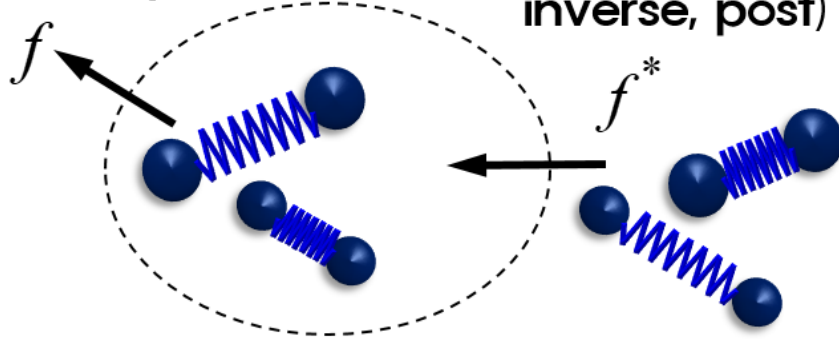
Argon gas
Mach 5.48
Knudsen 0.02



Argon gas
Mach 5.48
Knudsen 0.2

New nonlinear intramolecular interaction model

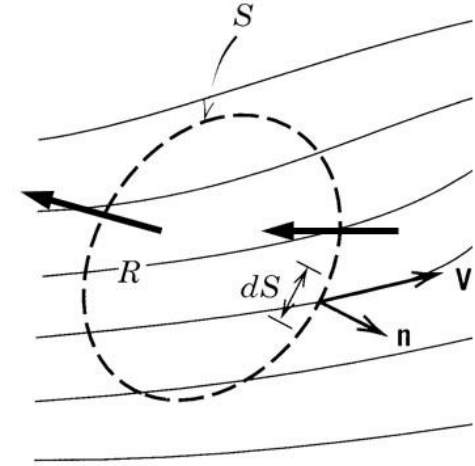
Loss (out of,
forward, pre)



$$\frac{\delta f}{\delta t} = C[f] = \text{Gain} - \text{Loss} = \frac{1}{2\lambda} (f^* - f)$$

**New nonlinear intramolecular interaction model
for the “spring” in the dumbbell**

When linearized, it reduces to $(f^{\text{eq}} - f) / \lambda$ (BGK model, 1954)



$$\frac{\partial}{\partial t} \int_R U dV = \text{In} - \text{Out} = \oint_S \mathbf{F} \cdot (-\mathbf{n}) dS$$

Conservation in control volume

Preprint (2023): A Boltzmann-type kinetic intramolecular model and its application to viscoelastic fluids

Boltzmann-type intramolecular interaction model

A molecular-level equation of the marginal probability density function of finding a dumbbell in the configuration vector space \mathbf{r} connecting two beads for a given time, $f(\mathbf{r}, t)$ (ζ friction coefficient, \mathbf{s} spring force, $\lambda \equiv \zeta / 4S_0$ relaxation)

$$\frac{\partial f}{\partial t} + \nabla \cdot \left((\nabla \mathbf{u})^T \mathbf{r} - \frac{2k_B T}{\zeta} \nabla \right) f = \nabla \cdot \left(\frac{2\mathbf{s}}{\zeta} f \right) \quad \text{Fokker-Planck}$$

$\mathbf{s} = S_0 \mathbf{r}$: Linear Hookean

$$\frac{\partial f}{\partial t} + \nabla \cdot \left((\nabla \mathbf{u})^T \mathbf{r} - \frac{2k_B T}{\zeta} \nabla \right) f = \frac{1}{2\lambda} (f^* - f) \quad \text{New Boltzmann-type}$$

Note that the interaction occurs through the "spring" in the dumbbell.

For the dumbbell models the forces on the two beads are equal and opposite, leading to a connector force.

Corresponding second-order constitutive model

Nonequilibrium entropy Ψ : $\Psi(\mathbf{r}, t) = -k_B \langle [\ln f(\mathbf{v}, \mathbf{r}, t) - 1] f(\mathbf{v}, \mathbf{r}, t) \rangle$,

Nonequilibrium entropy production:

$$\sigma_c \equiv -k_B \langle \ln f \mathcal{C}[f] \rangle = \frac{1}{4\lambda} k_B \langle \ln(f^*/f)(f^* - f) \rangle \geq 0 \text{ (satisfying 2nd-law)}$$

since $\ln(x/y)(x-y) \geq 0$.

$$\sigma_c = \frac{1}{4\lambda} k_B \langle f^{(0)}(x-y)[\exp(-y) - \exp(-x)] \rangle = \kappa_1 q(\kappa_1^{(\pm)}, \kappa_2^{(\pm)}, \dots) \text{ via cumulant expansion}$$

$$\sigma_c \equiv -k_B \langle \ln f \mathcal{C}[f] \rangle = \frac{1}{T} \sum_{n=1}^{\infty} X^{(n)} \langle h^{(n)} \mathcal{C}[f] \rangle = \frac{1}{T} \sum_{l=1}^{\infty} X^{(n)} \Lambda^{(n)},$$

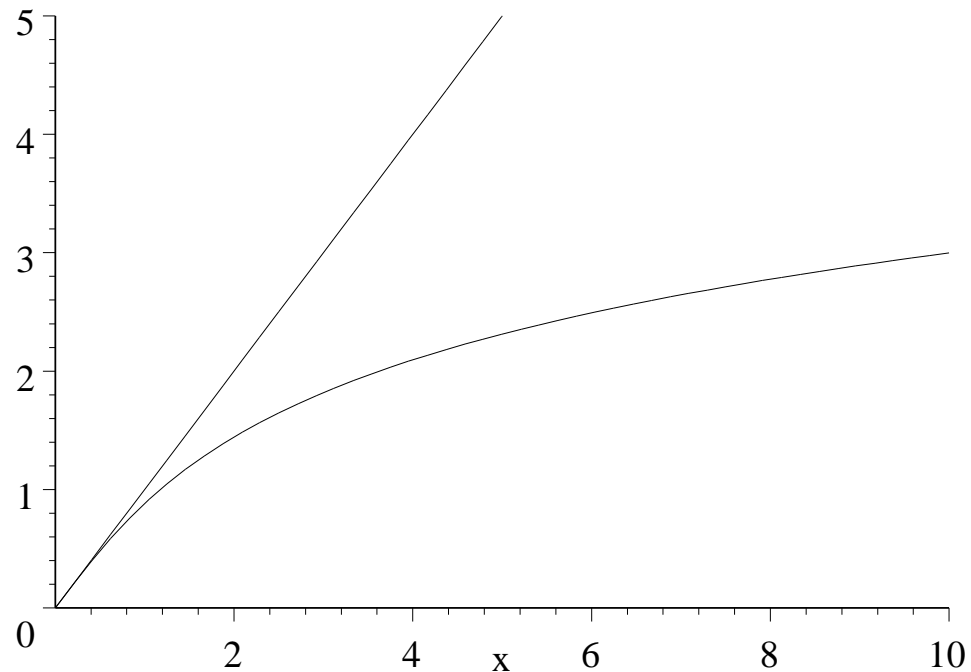
a thermodynamically-consistent constitutive equation can be derived;

$$\frac{D\boldsymbol{\tau}}{Dt} - [(\nabla \mathbf{u})^T \boldsymbol{\tau} + \boldsymbol{\tau} \nabla \mathbf{u}] - \frac{\mu}{\lambda} (\nabla \mathbf{u}^T + \nabla \mathbf{u}) = -\frac{1}{\lambda} \boldsymbol{\tau} q_{2\text{nd}}(\kappa_1),$$

$$q_{2\text{nd}}(\kappa_1) = \frac{\sinh \kappa_1}{\kappa_1}, \quad \kappa_1 = \alpha \frac{\sqrt{\boldsymbol{\tau} : \boldsymbol{\tau}}}{\mu / \lambda} \quad (\boldsymbol{\tau} \equiv nS_0 \langle \mathbf{r} \mathbf{r} f \rangle - nk_B T \mathbf{I})$$

2nd-order extension of Hooke's Law in elasticity

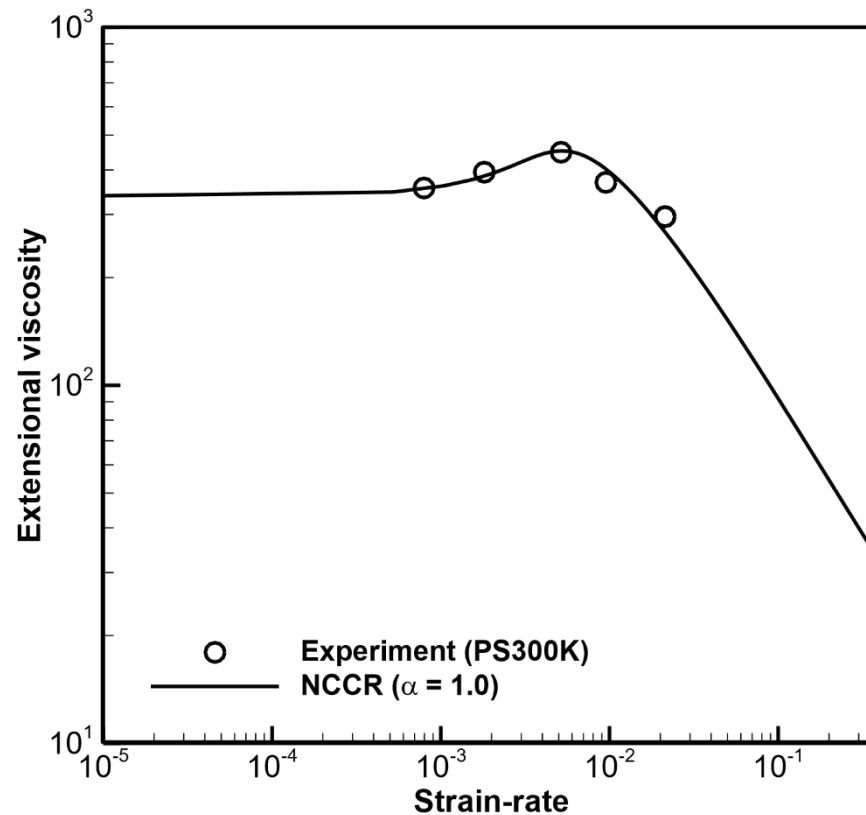
$$-\frac{\mu}{\lambda}(\nabla\mathbf{u}^T + \nabla\mathbf{u}) = -\frac{1}{\lambda}\boldsymbol{\tau}\frac{\sinh\kappa_1}{\kappa_1}, \quad \kappa_1 = \alpha\frac{\sqrt{\boldsymbol{\tau}:\boldsymbol{\tau}}}{\mu/\lambda}$$
$$\Rightarrow \hat{\boldsymbol{\tau}} = \frac{\sinh^{-1}(\alpha\hat{\boldsymbol{\tau}}_0)}{\alpha}$$



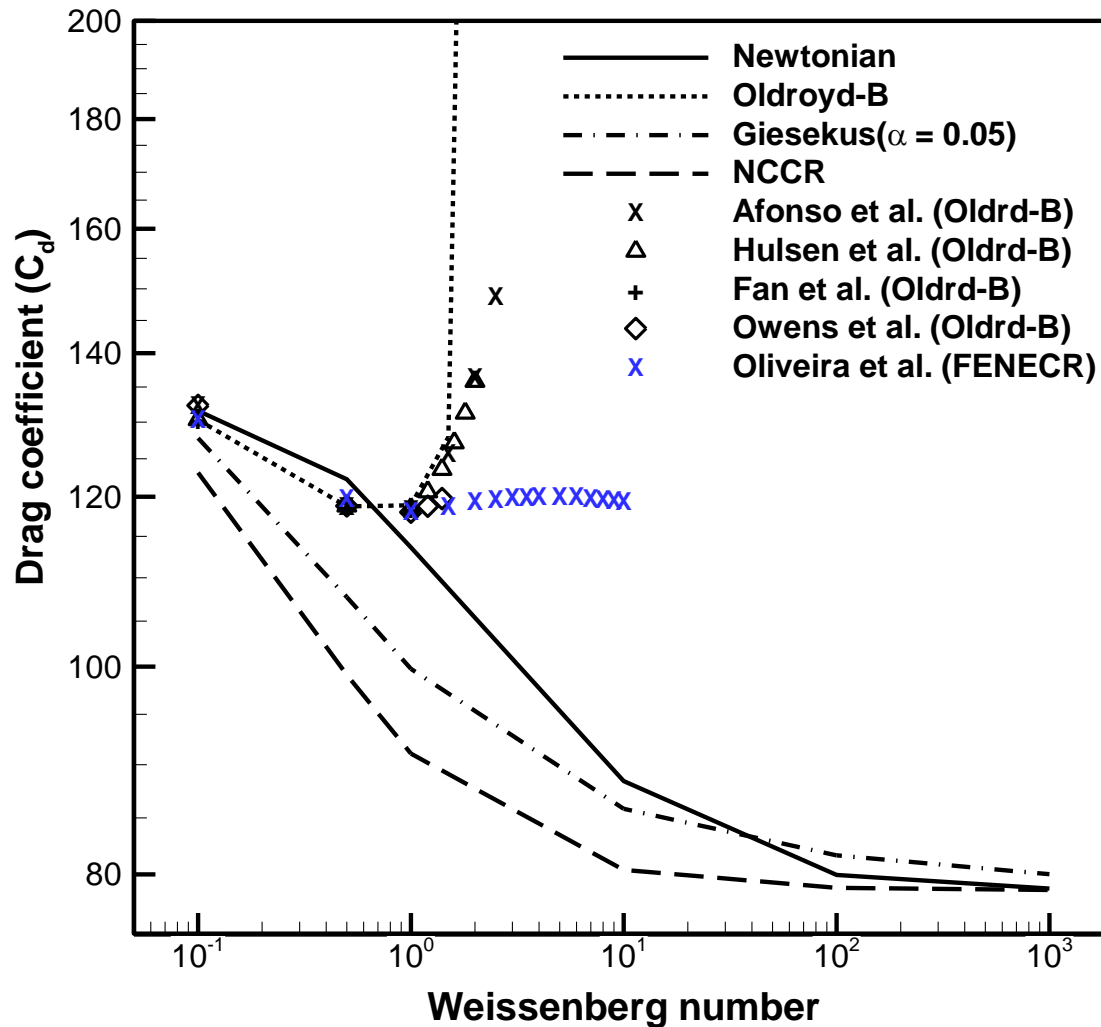
Application to viscoelastic fluids

$$\rho \frac{D\mathbf{u}}{Dt} + \nabla p + \mu_s \nabla^2 \mathbf{u} - \nabla \cdot \boldsymbol{\tau} = 0$$

$$\frac{D\boldsymbol{\tau}}{Dt} - [(\nabla \mathbf{u})^T \boldsymbol{\tau} + \boldsymbol{\tau} \nabla \mathbf{u}] - \frac{\mu}{\lambda} (\nabla \mathbf{u}^T + \nabla \mathbf{u}) = -\frac{1}{\lambda} \boldsymbol{\tau} \frac{\sinh \kappa_1}{\kappa_1}, \quad \kappa_1 = \alpha \frac{\sqrt{\boldsymbol{\tau} : \boldsymbol{\tau}}}{\mu / \lambda}$$



Computational simulation of viscoelastic fluids



Implementation
of the new
model to
viscoelastic
OpenFOAM
(cylinder flow)

Viscoelastic fluids: Barus effect in die swell



We = 2.5

We = 5.0

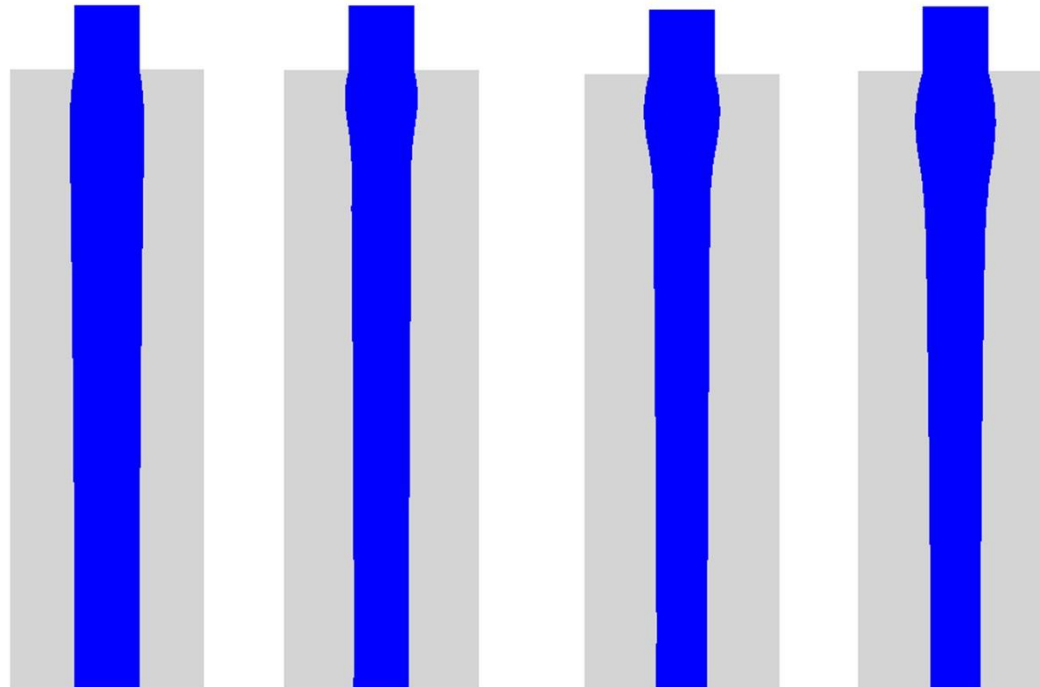
We = 10.0

(a)

(b)

(c)

(d)



Newtonian

New

New

New

Concluding remarks

Proposal of a new Boltzmann-type kinetic spring model

$$\frac{1}{2\lambda}(f^* - f) \quad \text{Cf.} \quad \frac{1}{\lambda}(f^{(0)} - f)$$

BGK (1954)
Yamamoto (1956), Lodge (1964), Modified network model

Second-order extension of Hooke's law in elasticity

$$\hat{\tau} = \frac{\sinh^{-1}(\alpha \hat{\tau}_0)}{\alpha}$$

Application to viscoelastic fluids

Similarities between rarefied gases and viscoelastic fluids